

HAYES HIGGINS PARTNERSHIP CHARTERED ENGINEERS • PROJECT MANAGERS

Civil Engineering Services Report For

Proposed Traveller-Specific Group Housing, Stockhole Lane

Co. Dublin



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DOCUMENT CONTROL SHEET

Client		Fingal	County	Counc	il				
Project T	itle			eller-Sp e, Co D		Group H	ousing,		
Project F	lef.	18D083 Planning Report							
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Revision	Status	Author	Reviewed By	Approved By	Issue Dates
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1. Introduction

Hayes Higgins Partnership has been commissioned to prepare a Civil Engineering Services Report for the proposed development at Stockhole Lane, Co. Dublin.

This report was compiled after reviewing the available information on drainage and water supply, reviewing the OPW flood maps and other available information from public bodies. It contains information on the design of the surface water and foul drainage systems to be constructed for the proposed development.

The design of both the surface water and foul drainage systems has been carried out in accordance with the following:

- The Greater Dublin Regional Code of Practice for Drainage Works
- Technical Guidance Document H of the Building Regulations
- The Greater Dublin Strategic Drainage Study (GDSDS)
- DOE Recommendations for Site Development Works for Housing Areas
- BS 8301:1985, Code of practice for Building Drainage
- BS EN 752 External building drainage
- OPW The Planning System and Flood Risk Management

The proposed surface water drainage system is a gravity feed drainage system discharging to a modular attenuation system in the south of the site. The surface water system is designed to take the runoff generated by a 1 in 100 year storm event (+20% climate change). The modular attenuation system will be connected to the existing surface water system which discharges into an existing water stream that discharges to the Sluice River at a point north of Baskin Lane (the L2055), to the west of the Malahide Road (the R107). A petrol interceptor tank will be provided between manhole \$03 and \$06. One existing manhole (downstream manhole \$07) and the existing pipe need to be modified in order to discharge at the existing level of the headwall invert level. A hydrobrake is to be used to limit max discharge to 3.11 I/s (Qbar), which is the maximum allowable site discharge.

The foul drainage system for the proposed development is a gravity feed system within the site falling to the existing public foul drainage system, Cloghran Sewer. Also, the existing 10 dwellings at Baskin Park & Court will be connected to this sewer by modifying the existing pump chamber to become outfall manhole, installing a new foul sewer and manhole. The existing waste water treatment plant will be decommissioned.

2. Proposed Site

The site in question is a green field site which measures approximately 1.22ha in area. Originally, it was used for agriculture. It is located to the east of Stockhole Lane. An existing residential development Baskin Court and Baskin Park is situated to the north, and agricultural fields to the east and south. The site is bounded by a palisade fence. A series of earth mounds are present on the land. The site also contains a waste water treatment plant and percolation for 10 existing dwellings at Baskin Court and Baskin Park.

Proposed on the site are seven dwellings as Traveller-Specific Group Housing and associated site development works. The dwellings will back onto the east boundary and face the proposed public open space and Stockhole Lane to the west. The houses are bungalows. There is a high point in the south-east corner of the road and a low point in the north. Each car parking and footpath falls away from the finish floor levels by 2% to eastern side of the new road where new gullies are to be installed. The road crossfall goes from the western side of the road to the eastern by 2%. The houses will be accessed directly from the proposed road to the front.



3. Surface Water Drainage

Local Authorities require that all developments must include a sustainable urban drainage system, SuDS.

The conditions on site are not favourable to infiltration as stated in Stockhole Lane –Ground Investigation Interpretative Report (18-1309) carried out by CausewayGeotech. Soakaways tests were carried out (trial pit SA01–SA03) according to the Building Research Establishment (2007), BRE Digest 365: Soakaways. As a result, the absence of outflow from the pits indicated very low infiltration coefficients. The low-permeability fine-grained soils are therefore considered to have limited infiltration and would be deemed unsuitable for the implementation of infiltration drainage systems. The ground has no capacity (no infiltration) to accept water discharge because of its low permeability, which will cause water retention instead of promoting water flow for recharging. For these reasons, the use of swales, infiltration trenches, permeable paving and soakaways are ineffective. A retention basin was proposed at an early stage, however, it was considered hazardous due to its depth (2-2.5m), and also there is a risk it would be used as a landfill site.

Taking into account this, a surface water attenuation system connected to the existing surface drainage network, via a hydrobrake limiting discharge to 3.11 I/s (Qbar), is to be used to dispose of the surface water from the developed site to an existing water stream.

The gravity feed surface water system will serve the hardstanding on site. The main surface sewers in the proposed development are to consist of 225mm diameter uPVC pipes with fall 1/200, with the exceptions of two pipelines that need to be 300mm diameter. One pipeline from surface manhole S03 to the Petrol Interceptor Tank, and another new pipeline from the existing manhole to be modified to the existing headwall, which will also receive discharge from the existing 10 dwellings at Baskin Park & Court. Given the levels on site the simplest approach is to use one attenuation system. The total impermeable surface area is the sum of roofs, footpaths, paving and road areas, which results in 2301 m². Surface water sewers will fall by gravity to the proposed attenuation system located in the south. The attenuation system will connect via hydrobrake to the existing surface water sewer, which has to be modified to comply with the new invert levels required.

The existing surface water sewer to be modified is located within a 10m wide and it falls downslope away from the site. It is proposed to upsize the pipe from the existing 225mm diameter pipe to a 300mm diameter pipe due to capacity requirements taking into account the increased loading due to collection of surface water from 2301sqm of impermeable surface that was previously greenfield. Also, it is being taken into account the surface water discharge from 10 dwellings Baskin Park & Court by a 100mm diameter rising main into an existing manhole to be modified (S08) just downstream the new surface manhole S07.

The required storage volume to retain the on-site runoff for the group of houses is noted on drainage drawing 01. To alleviate any possible risk of flood the storage is designed for a 1 in 100 year storm (+20%). A 20% increase in runoff due to global warming is included as per "Greater Dublin Regional Code of Practice for Drainage Works" and the "GDSDS".

The surface water drains have been designed in accordance with BS EN 752, Code of Practice for Drainage Outside Buildings. Details of the proposed surface water drainage system are shown in Hayes Higgins Partnership drawing 01 and calculations within Appendix A.



4. Foul Water Drainage

The foul drainage system has been designed in accordance with BS 8301:1985, Code of Practice for Building Drainage and the current Building Regulations.

The foul drainage system for the development is a gravity feed system falling to an existing 225mm diameter foul sewer located to the west of the site, on Stockhole Lane (the Cloghran Sewer). Foul sewers from the development will be connected to this foul sewer via new pipe infrastructure and will eventually discharge to the Ringsend Wastewater Treatment Plant (WWTP) for treatment and ultimate disposal. The development will not result in a significant increase in foul discharge (peak flow of 0.294 I/s) from the site on the public sewer and we do not anticipate any capacity problems.

Average flow = 600 I/day per dwelling = 0.007 I/s

7 no. dwellings = 0.049 l/s

Peak flow = 6xDry weather flow (average flow) = $6 \times 0.049 = 0.294$ l/s

The main foul sewers in the proposed development are to consist of 225mm diameter concrete pipes with fall 1/200 chosen throughout to minimise the risk of blockages and to aid maintenance. Based on the 225mm diameter pipes with a 1:200 fall, the design flow is calculated as 32.18 l/s. The achieved velocity is 0.81 m/s, which is higher than the minimum self-cleansing velocity of 0.75 m/s for pipes less than 300mm diameter. A roughness coefficient (ks) of 1.5mm is applied to the design of all pipes.

The drawings included with the planning application show the proposed foul drainage layout. Details of the proposed foul sewer are shown in Hayes Higgins Partnership drawing 01 and calculations within Appendix B.

5. Water Supply System

There is an existing watermain located in Baskin Court. It is proposed to extend the watermain with a 100mm diameter HDPE watermain pipe through the site to serve the proposed houses.

In accordance with requirements air valves and scour valves will be provided around the site as necessary. Hydrants will be provided as directed by the Fire Safety Certificate and Technical Guidance Document B of the Building Regulations 2006. Water saving devices including aerated taps and low water usage appliances will be used in the proposed development in accordance with best practice. The proposed watermain layout and details are shown on Hayes Higgins Partnership drawing 03.

6. Stage 1 Flood Risk Assessment

A stage 1 desktop flood risk assessment was undertaken to identify possible sources of flooding and the risk posed to the development, and separately the risk posed to surrounding areas as a result of the development. The Guidelines for Planning Authorities – The Planning System and Flood Risk Management was referenced during design.



Tidal

The site is situated far enough away from the sea not to be subjected to coastal or tidal flooding.

Fluvial, Pluvial (urban drainage), and pluvial (overland flow)

External Sources

The OPW flood mapping website, <u>www.floodmaps.ie and www.floodinfo.ie have</u> been reviewed and included in Appendix E. Both websites show some flooding downstream the water stream mentioned, however, the site is located at a higher level than the water stream and the surrounding land slopes away from the site. Also, from the information contained in this report it is evident that the site has not been subjected to flooding during previously reported flooding events as consulted the websites above. As such it is reasonable to assume there is no risk to the proposed development resulting from flooding off-site.

Internal sources

It is intended that all surface water run off generated by the 1in100 year storm will be dealt with via the attenuation tank. An allowance has been made for a 20% increase in runoff due to global warming, as per the "Greater Dublin Strategic Drainage Study" recommendations.

Blockages

All dwellings have a 2% downhill gradient towards the road where the surface water is taken and discharge into an existing water stream. The site also has a downhill gradient south towards the existing water stream mentioned above. The adjacent public sewers are running down the slope away from the site.

Groundwater

Groundwater was encountered deeply in 4 tests of 12. The site also has a downhill gradient south towards the existing water stream apart the proposed dwellings.

Due to all of these factors the risk of flooding is minimal.

A Stage 2 FRA is currently being complete by IE Consulting.

7. Site Access

Vehicular access to the houses will be provided from the extension of the existing road, Stockhole Lane. There will be a raised table for pedestrian crossing and speed control. The housing development will also be reachable by foot from existing footpath in the north which will be connected to a new footpath between green area and the new road. This new footpath will lead to the dwellings. At all pedestrian crossing points tactile paving will be provided. Sufficient corner radii bends, site distances at junctions, road widths (6m width) and footpaths widths (2m width) will be provided throughout. Road layout complies with Design Manual for Urban Roads. Each dwelling is going to have 2 parking spaces. Sufficient sightlines are provided at the exit from the site onto Stockhole Lane as shown in Hayes Higgins Partnership drawing 04.

8. Services Design Summary

The proposed Surface water drainage system has been set up so as to ensure that adequate selfcleansing velocities are obtained, in accordance with the Building Regulations, and to comply in full with the Greater Dublin Regional Code of Practice for Drainage Works. Similarly, the proposed Foul drainage system has been set up to ensure that adequate self-cleansing velocities are obtained for partial flows under design loading, in accordance with the Building Regulations.



Appendix A

Job Title:	STOCKHOLE LANE	Job Number:	18D073
Calculation by:	JGC	Date:	03.08.19
Checked by:			

																			Q	
Sewer	Cover	Invert	Depth	Cover	Length	Gradient	Pipe	Velocity	Pipe	Time Of	Time Of	Rate Of	IMPERMEABLE AREA			Required Pipe				
Ref Number	Level	Level	To Manhole				Diameter	flowing full	Capacity	Flow	Concentration	Rainfall	Roof	Road	Footpath	Paving	Total	Cumulative	Rate Of Flow	Capacity
	(m)	(m)	(m)	(m)	(m)	(1 in)	(mm)	(m/s)	(l/s)	(min)	(min)	(mm/hr)	(m^2)	(m^2)	(m^2)	(m^2)	(m^2)	(m^2)	(l/s)	(I/s)
S01	46.30	45.13	1.17				225													
S01-S02	46.53	45.04	1.49	1.26	18.6	200	225	0.92	36.55	0.34	5.34	76.8	377	235	51	50	688	688	14.7	36.5
S02-S03	46.93	44.83	2.10	1.88	41.2	200	225	0.92	36.55	0.75	6.09	71.0	120	169	56	50	370	1058	20.9	36.5
S04	47.09	45.06	2.03	1.81			225													
S04-S05	47.07	44.97	2.10	1.87	18.3	200	225	0.92	36.55	0.33	5.33	76.8	258	248	50	50	581	581	12.4	36.5
S05-S03	46.93	44.83	2.10	1.88	28.2	200	225	0.92	36.55	0.51	5.84	72.7	119	451	80	25	662	1242	25.1	36.5
S03	46.93	44.83	2.10	1.88			225													
S03-S06	46.32	44.50	1.82	1.52	47.4	200	300	1.11	78.21	0.71	5.71	73.7	874	1103	237	175	2301	2301	47.1	78.2
S07	46.70	44.39	2.31	2.09			225			4.1/-										
S07-S08	47.90	44.35	3.55	3.33	35.6	200		FLOW CON	$11 \text{ KOL} = 3.1^{\circ}$	1 1/5										
	Ref umber \$\$01 \$\$01-\$02 \$\$2-\$03 \$\$04 \$\$04-\$05 \$\$5-\$03 \$\$03 \$\$3-\$506 \$\$07	Ref umber Level 000 (m) 501 46.30 01-502 46.53 02-503 46.93 504 47.09 04-505 47.07 05-503 46.93 503 46.93 303-606 46.32 507 46.70	Ref umber Level Level (m) (m) S01 46.30 45.13 D1-S02 46.53 45.04 D2-S03 46.93 44.83 S04 47.09 45.06 D4-S05 47.07 44.97 D5-S03 46.93 44.83 S03 46.93 44.83 S07 46.70 44.39	Ref umber Level Level To Manhole (m) (m) (m) S01 46.30 45.13 1.17 D1-S02 46.53 45.04 1.49 02-S03 46.93 44.83 2.10 S04 47.09 45.06 2.03 94-S05 47.07 44.97 2.10 95-S03 46.93 44.83 2.10 90 50.6 46.93 44.83 2.10 90 46.93 44.83 2.10 10 90 46.93 44.83 2.10 10 903 46.93 44.83 2.10 10 903 46.93 44.83 2.10 10 903 46.93 44.39 2.31 10	Ref umber Level To Manhole (m) (m) (m) S01 46.30 45.13 1.17 D1-S02 46.53 45.04 1.49 1.26 02-S03 46.93 44.83 2.10 1.88 504 47.09 45.06 2.03 1.81 04-S05 47.07 44.97 2.10 1.87 05-S03 46.93 44.83 2.10 1.88 S03 46.93 44.83 2.10 1.88 S07 46.70 44.39 2.31 2.09	Ref umber Level Level 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Appendix B

<u>Job Title:</u>	STOCKHOLE LANE	<u>Job Number:</u>	18D073
Calculation by:	JGC	Date:	13.12.18
Checked by:			

Proposed Foul Drainage Design

Manhole Ref Number	Sewer Ref Number	Cover Level (m)	Invert Level (m)	Depth To Manhole (m)	Length (m)	Gradient (1 in)	Pipe Diameter (mm)	Velocity flowing full (m/s)	Pipe Capacity (I/s)
F01		47.00	44.70	2.31					
F02	F01-F02	47.04	44.58	2.47	23.8	200	225	0.81	32.18
F03	F02-F03	46.93	44.41	2.52	32.7	200	225	0.81	32.18
F04		46.19	44.73						
F03	F04-F03	46.93	44.41	2.52	63.0	200	225	0.81	32.18
F03		46.93	44.41	2.52					
F05	F03-F05	47.15	44.21	6.66	39.8	200	225	0.81	32.18
Ex.F.MH		44.30	41.95	2.35					
F06	Ex.F.MH-F06	44.60	40.50	4.10	10.0	200.00	225	0.81	32.18

Appendix C



Calculated by:	Jacob Granados				
Site name:	Stockhole Lane				
Site location:	Stockhole Lane, Co. Dublin				

This is an estimation of the greenfield runoff rate limits that are needed to meet normal best practice criteria in line with Environment Agency guidance "Preliminary rainfall runoff management for developments", W5-074/A/TR1/1 rev. E (2012) and the SuDS Manual, C753 (Ciria, 2015). This information on greenfield runoff rates may be the basis for setting consents for the drainage of surface water runoff from sites.

Greenfield runoff estimation for sites

www.uksuds.com | Greenfield runoff tool

Site coordinates

Latitude:	53.42312° N
Longitude:	6.21231° W
Reference:	6519204
Date:	2019-01-24T12:03:58

Methodology	IH124								
Site characteristics									
Total site area (ha)		1.22							
Methodology									
Qbar estimation metho	bd	Calculate fro	om SPR a	nd SAAR					
SPR estimation metho	om SOIL type								
	Default	Edited							
SOIL type			2	2					
HOST class									
SPR/SPRHOST			0.3	0.3					
Hydrological charact	eristic	s	Default	Edited					
SAAR (mm)			933	933					
Hydrological region			12	12					
Growth curve factor: 1	0.85	0.85							
Growth curve factor: 3	2.13	2.13							
Growth curve factor: 1	00 ye	ar	2.61	2.61					

Notes:

(1) Is Q_{BAR} < 2.0 l/s/ha?

(2) Are flow rates < 5.0 l/s?

Where flow rates are less than 5.0 l/s consents are usually set at 5.0l/s if blockage from vegetation and other materials is possible. Lower consent flow rates may be set in which case blockage work must be addressed by using appropriate drainage elements

(3) Is SPR/SPRHOST ≤ 0.3 ?

Where groundwater levels are low enough the use of soakaways to avoid discharge offsite may be a requirement for disposal of surface water runoff.

Greenfield runoff rates	Default	Edited
Qbar (l/s)	3.11	3.11
1 in 1 year (l/s)	2.65	2.65
1 in 30 years (l/s)	6.63	6.63
1 in 100 years (l/s)	8.12	8.12

This report was produced using the greenfield runoff tool developed by HR Wallingford and available at www.uksuds.com. The use of this tool is subject to the UK SuDS terms and conditions and licence agreement, which can both be found at http://uksuds.com/terms-and-conditions.htm. The outputs from this tool have been used to estimate storage volume requirements. The use of these results is the responsibility of the users of this tool. No liability will be accepted by HR Wallingford, the Environment Agency, CEH, Hydrosolutions or any other organisation for use of this data in the design or operational characteristics of any drainage scheme.

Appendix D

Met Eireann Return Period Rainfall Depths for sliding Durations Irish Grid: Easting: 318618, Northing: 243851,

	Interval						Years								
DURATION	6months, lyear,	2,	З,	4,	5,	10,	20,	30,	50,	75,	100,	150,	200,	250,	500,
5 mins	2.5, 3.5,	4.0,	4.8,	5.3,	5.7,	7.1,	8.7,	9.7,	11.1,	12.4,	13.4,	14.9,	16.1,	17.1,	N/A ,
10 mins	3.4, 4.8,	5.6,	6.7,	7.4,	8.0,	9.9,	12.1,	13.5,	15.5,	17.3,	18.7,	20.8,	22.4,	23.8,	N/A ,
15 mins	4.0, 5.7,	б.5,	7.8,	8.7,	9.4,	11.7,	14.2,	15.9,	18.2,	20.3,	22.0,	24.5,	26.4,	28.0,	N/A ,
30 mins	5.3, 7.4,	8.5, 1	10.1,	11.2,	12.0,	14.8,	17.9,	19.9,	22.7,	25.2,	27.1,	30.1,	32.4,	34.3,	N/A ,
1 hours	7.0, 9.6,	11.0, 1	13.0,	14.4,	15.4,	18.7,	22.5,	24.9,	28.3,	31.3,	33.6,	37.1,	39.8,	42.0,	N/A ,
2 hours	9.3, 12.6,	14.3, 1	16.7,	18.4,	19.7,	23.8,	28.3,	31.2,	35.2,	38.8,	41.5,	45.6,	48.8,	51.4,	N/A ,
3 hours	11.0, 14.7,	16.6, 1	19.4,	21.3,	22.7,	27.3,	32.3,	35.6,	40.1,	44.0,	47.0,	51.5,	55.0,	57.9,	N/A ,
4 hours	12.3, 16.4,	18.5, 2	21.6,	23.6,	25.2,	30.1,	35.6,	39.1,	43.9,	48.1,	51.3,	56.2,	59.9,	63.0,	N/A ,
6 hours	14.5, 19.1,	21.5, 2	25.0,	27.3,	29.0,	34.6,	40.7,	44.5,	49.9,	54.5,	58.1,	63.4,	67.5,	70.9,	N/A ,
9 hours	17.1, 22.3,	25.1, 2	29.0,	31.6,	33.5,	39.7,	46.5,	50.8,	56.7,	61.9,	65.8,	71.6,	76.1,	79.8,	N/A ,
12 hours	19.1, 24.9,	27.9, 3	32.2,	35.0,	37.1,	43.8,	51.1,	55.8,	62.1,	67.6,	71.8,	78.1,	82.9,	86.8,	N/A ,
18 hours	22.5, 29.1,	32.5, 3	37.3,	40.5,	42.8,	50.4,	58.5,	63.6,	70.6,	76.7,	81.3,	88.2,	93.4,	97.7,	N/A ,
24 hours	25.3, 32.5,	36.2, 4	41.4,	44.9,	47.4,	55.6,	64.3,	69.8,	77.4,	83.9,	88.8,	96.1,	101.7,	106.3,	121.7,
2 days	31.4, 39.6,	43.7, 4	49.5,	53.3,	56.1,	65.0,	74.4,	80.3,	88.2,	95.1,	100.2,	107.9,	113.6,	118.3,	134.2,
3 days	36.3, 45.3,	49.7, 5	56.0,	60.1,	63.1,	72.6,	82.5,	88.7,	97.1,	104.3,	109.6,	117.6,	123.6,	128.5,	144.8,
4 days	40.6, 50.2,	55.0, 6	61.7,	66.0,	69.2,	79.2,	89.6,	96.1,	104.9,	112.3,	117.8,	126.1,	132.3,	137.3,	154.1,
6 days	48.1, 58.8,	64.1,	71.5,	76.2,	79.7,	90.6,	101.9,	108.9,	118.2,	126.2,	132.1,	140.8,	147.4,	152.7,	170.3,
8 days	54.7, 66.4,	72.1, 8	80.1,	85.1,	88.9,	100.5,	112.5,	120.0,	129.9,	138.2,	144.4,	153.6,	160.5,	166.0,	184.4,
10 days	60.7, 73.3,	79.4, 8	87.9,	93.2,	97.2,	109.5,	122.2,	130.0,	140.3,	149.1,	155.6,	165.2,	172.3,	178.1,	197.1,
12 days	66.3, 79.7,	86.1, 9	95.1,	100.7,	105.0,	117.8,	131.1,	139.2,	150.0,	159.1,	165.8,	175.8,	183.2,	189.1,	208.8,
16 days	76.7, 91.5,	98.5, 10	08.3,	114.5,	119.1,	133.0,	147.3,	156.0,	167.6,	177.3,	184.5,	195.1,	202.9,	209.2,	230.1,
20 days	86.3, 102.3,	109.9, 12	20.4,	127.0,	132.0,	146.8,	162.0,	171.3,	183.6,	193.8,	201.4,	212.5,	220.8,	227.4,	249.2,
25 days	97.6, 114.9,	123.2, 13	34.5,	141.6,	146.9,	162.8,	179.0,	188.9,	201.9,	212.7,	220.7,	232.5,	241.2,	248.2,	271.1,
NOTES:															

N/A Data not available

These values are derived from a Depth Duration Frequency (DDF) Model

For details refer to:

'Fitzgerald D. L. (2007), Estimates of Point Rainfall Frequencies, Technical Note No. 61, Met Eireann, Dublin', Available for download at www.met.ie/climate/dataproducts/Estimation-of-Point-Rainfall-Frequencies_TN61.pdf

	1	2	3	4	5	6
Time	Storm Frequency & Duration	Rainfall	Rainfall Intensity	Potential Run-off From Developed Site	Allowable Run- off From Developed Site	Storage Requirement
(mins)		(mm)	(mm/hr)	(l/s)	(I/s)	(m3)
5	M30-5 min	9.70	116.40	74.40	3.11	21.4
10	M30-10 min	13.50	81.00	51.77	3.11	29.2
15	M30-15 min	15.90	63.60	40.65	3.11	33.8
30	M30-30 min	19.90	39.80	25.44	3.11	40.2
60	M30-60 min	24.90	24.90	15.92	3.11	46.1
120	M30-2 hr	31.20	15.60	9.97	3.11	49.4
180	M30-3 hr	35.60	11.87	7.58	3.11	48.3
240	M30 - 4hr	39.10	9.78	6.25	3.11	45.2
360	M30-6 hr	44.50	7.42	4.74	3.11	35.2
540	M30-9 hr	50.80	5.64	3.61	3.11	16.1
<u>720</u>	<u>M30-12 hr</u>	<u>55.80</u>	<u>4.65</u>	<u>2.97</u>	<u>3.11</u>	<u>-6.0</u>
1080	M30-18 hr	63.60	3.53	2.26	3.11	-55.2
1440	M30-24 hr	69.80	2.91	1.86	3.11	-108.1
2880	M30-2day	80.30	1.67	1.07	3.11	-352.6

15D086 - Surface Water Attenutation Calculation 1-30

17D004 - Surface Water Attenutation Calculation 1-100 + 20%

1	2	3	4	5	6
Storm Frequency & Duration	Rainfall	Rainfall Intensity	Potential Run-off From Developed Site	Allowable Run- off From Developed Site	Storage Requirement
	(mm)	(mm/hr)	(l/s)	(l/s)	(m3)
M100-5 min	16.08	192.96	123.33	3.1	36.1
M100-10 min	22.44	134.64	86.06	3.1	49.8
M100-15 min	26.40	105.60	67.50	3.1	57.9
M100-30 min	32.52	65.04	41.57	3.1	69.2
M100-60 min	40.32	40.32	25.77	3.1	81.6
M100-2 hr	49.80	24.90	15.92	3.1	92.2
M100-3 hr	56.40	18.80	12.02	3.1	96.2
M100 - 4hr	61.56	15.39	9.84	3.1	96.9
M100-6 hr	69.72	11.62	7.43	3.1	93.2
M100-9 hr	78.96	8.77	5.61	3.1	80.9
M100-12 hr	86.16	7.18	4.59	3.1	63.9
M100-18 hr	97.56	5.42	3.46	3.1	23.0
<u>M100-24 hr</u>	<u>106.56</u>	<u>4.44</u>	<u>2.84</u>	<u>3.1</u>	<u>-23.5</u>
M100-2day	120.24	2.51	1.60	3.1	-260.7
Allowable Dup off	2 11				

Allowable Run-off3.11I/sTotal Area2301m²



User Inputs

Results

Outlet Control Structure Project Name Engineer Project Location Project Date Measurement Type Required Storage Volume Stone Porosity Stone Foundation Depth Stone Above Chambers Average Cover Over Chambers Design Constraint Design Constraint Dimension

Chamber Model

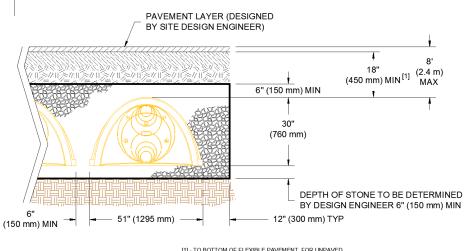
SC-740 Yes (Outlet) Proposed Housing, Stockhole Lane, Co. Dublin Jacob Granados Stockhole Lane, Co. Dublin 01/24/2019 Metric 97 cubic meters 40% 152 mm. 152 mm. 152 mm. 460 mm. Width 10 meters

System Volume and Bed Size

Installed Storage Volume	99 cubic meters
Storage Volume Per Chamber	2.12 cubic meters
Number Of Chambers Required	40 each
Number Of End Caps Required	12 each
Rows/Chambers	4 row(s) of 7 chamber(s)
Leftover Rows/Chambers	2 row(s) of 6 chamber(s)
Maximum Length	17.38 meters
Maximum Width	9.33 meters
Approx. Bed Size Required	158 square meters

System Components

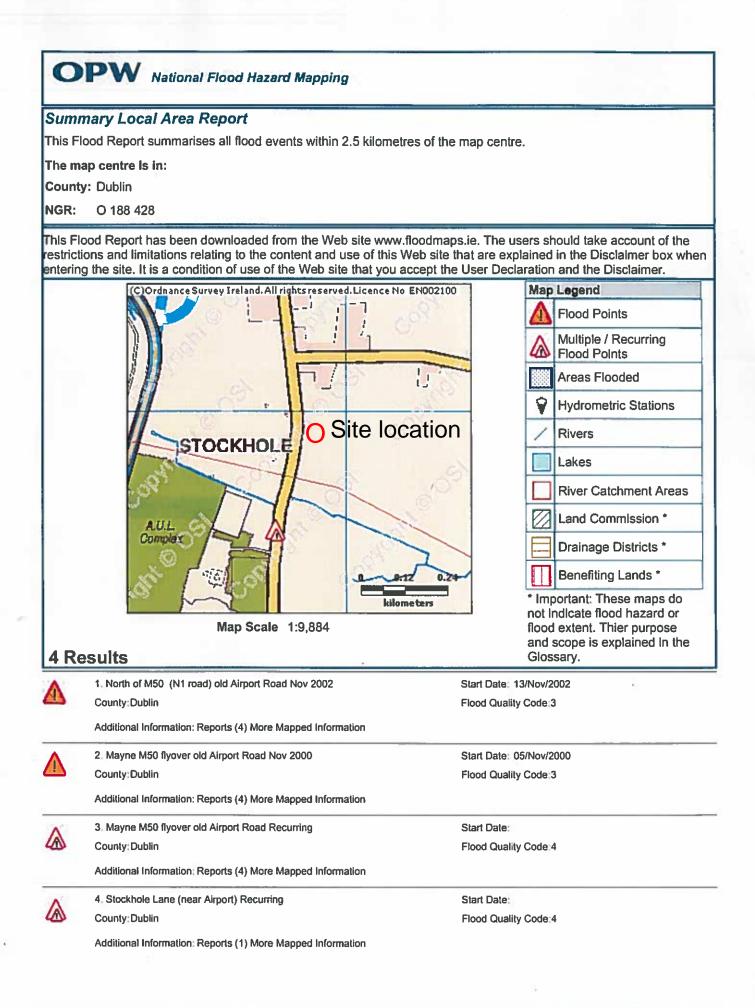
Amount Of Stone Required	116 cubic meters
Volume Of Excavation (Not Including Fill)	168 cubic meters
Non-woven Filter Fabric Required	370 square meters
Length Of Isolator Row	15.67 meters
Non-Woven Isolator Row Fabric	36 square meters
Woven Isolator Row Fabric	46 square meters



[1] - TO BOTTOM OF FLEXIBLE PAVEMENT. FOR UNPAVED INSTALLATIONS WHERE RUTTING FROM VEHICLES MAY OCCUR, INCREASE COVER TO 24" (600 mm).

© ADS Stormtech 2016

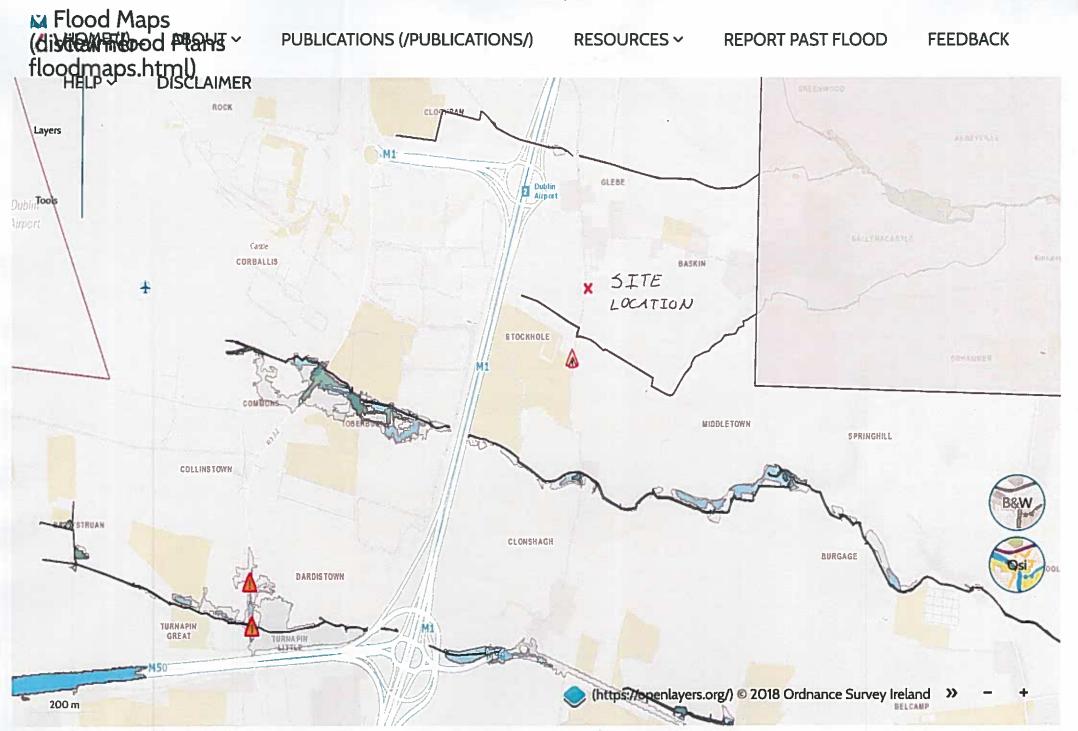
Appendix E



Report Produced: 13-Dec-2018 14:07



Flood Maps - Floodinfo.ie



Appendix F

SUDS/Green Infrastructure measures selected for this site

Suds Measures	Measures	Rationale for selecting/not selecting measure			
	to be				
	used on				
	this site				
Source Control	Source Control				
	N	Swales were ruled out due to adverse site topography; ground is			
		rising from the lowest dwelling (no 1) and associated road, at the			
		north of the site, whilst surface water drainage needs to fall in a			
		southerly direction. Last but not least the conditions on site are not favourable to			
		infiltration as stated in Stockhole Lane –Ground Investigation			
		Interpretative Report (18-1309). Soakaways tests were carried out			
		(trial pit SA01–SA03) according to the Building Research			
		Establishment (2007), BRE Digest 365: Soakaways. As a result, the			
Swales		absence of outflow from the pits indicated very low infiltration			
		coefficients. The low-permeability fine-grained soils are therefore			
		considered to have limited infiltration and would be deemed			
		unsuitable for the implementation of infiltration drainage systems. The ground has no capacity (no infiltration) to accept water			
		discharge because of its low permeability, which will cause water			
		retention instead of promoting water flow for recharging. For these			
		reasons, the use of swales are ineffective.			
		Refer to section 3 Surface Water Drainage of the Civil Engineering			
		Services Report.			
	N	Tree pits were ruled out due to adverse topography; open space			
		and trees are located on ground which is higher than the lowest			
		dwelling no 1 and associated road at the north of the site.			
		Last but not least firm/stiff glacial till at 1.5/2m depth means tree			
Tree Pits		pits are not suitable. The ground has no capacity (no infiltration) to			
		accept water discharge because of its low permeability, which will			
		cause water retention instead of promoting water flow for			
		recharging. For these reasons, the use of tree pits is ineffective.			
		Refer to section 3 Surface Water Drainage of the Civil Engineering Services Report.			
Rainwater Butts	N	Client Decision			
	N	Development is residential and too small to consider use of			
Rainwater harvesting		rainwater harvesting			
	N	Firm/Stiff glacial till at 1.5/2m depth means Soakaways are not			
Soakaways		suitable. 3 No. Infiltration tests indicated that the proposed site lies			
		within the extremely low permeability range.			
Infiltration trenches	N	Firm/Stiff glacial till at 1.5/2m depth means Infiltration trenches are			
		not suitable. 3 No. Infiltration tests indicated that the proposed site lies within the extremely low permeability range.			
	N	Firm/Stiff glacial till at 1.5/2m depth means Permeable pavement			
Permeable pavement		are not suitable. 3 No. Infiltration tests indicated that the proposed			
renneable pavement		site lies within the extremely low permeability range.			
	N	Firm/Stiff glacial till at 1.5/2m depth means Grasscrete are not			
- Grasscrete		suitable. 3 No. Infiltration tests indicated that the proposed site lies			
Plack paying	N				
- BIOCK PAVILIS					
	N				
- Porous Asphalt		suitable. 3 No. Infiltration tests indicated that the proposed site lies			
		within the extremely low permeability range.			
- Block paving	N N N	 Firm/Stiff glacial till at 1.5/2m depth means Grasscrete are not suitable. 3 No. Infiltration tests indicated that the proposed site lies within the extremely low permeability range. Firm/Stiff glacial till at 1.5/2m depth means Block paving are not suitable. 3 No. Infiltration tests indicated that the proposed site lies within the extremely low permeability range. Firm/Stiff glacial till at 1.5/2m depth means Porous Asphalt are not suitable. 3 No. Infiltration tests indicated that the proposed site lies within the extremely low permeability range. 			

Green Roofs	N	Housing unit design does not allow for green roofs
	Ν	Firm/Stiff glacial till at 1.5/2m depth means Filter strips are not
Filter strips		suitable. 3 No. Infiltration tests indicated that the proposed site lies
		within the extremely low permeability range.
	Ν	Firm/Stiff glacial till at 1.5/2m depth means Bioretention systems
Bioretention systems		are not suitable. 3 No. Infiltration tests indicated that the proposed
		site lies within the extremely low permeability range.
Blue Roofs	N	Housing unit design does not allow for blue roofs
Filter Drain	Ν	Firm/Stiff glacial till at 1.5/2m depth means Filter Drain are not
Filter Drain		suitable. 3 No. Infiltration tests indicated that the proposed site lies within the extremely low permeability range.
Site Control		
	Ν	An attenuation basin was considered and designed in the southern
		part of the site but this was ruled out due to excessive depth and
Detention Basins		associated risks of becoming a site for illegal dumping.
		Refer to HHP drawing number 01_Proposed Drainage Layout. Sheet 1 of 2_Rev P.
	N	An attenuation basin was considered and designed in the southern
	IN IN	part of the site but this was ruled out due to excessive depth and
Retentions basins		associated risks of becoming a site for illegal dumping.
		Refer to HHP drawing number 01_Proposed Drainage Layout. Sheet
		1 of 2_Rev P.
Regional Control		
Ponds	Ν	Green spaces are too small to facilitate ponds
Wetlands	Ν	Green spaces are too small to facilitate wetlands
Other		
Petrol/Oil interceptor	Y	Suitable for proposed development
Attenuation tank – only as a last	Y	A StormTech attenuation system is used which allows for infiltration
resort where other measures		of stormwater where possible.
are not feasible		
Oversized pipes- only as a last	Ν	Not required
resort where other measures		
are not feasible		

Note:

- 1. Fingal has a preference for above ground Green Infrastructure rather than tanks or over sized pipes . Above ground flows through swales, basins etc are encouraged.
- 2. Demonstrate SUDS system will have sufficient Pollutant removal efficiency in accordance with Ciria Suds Manual C753
- 3. Basins sides should be no steeper than 1:4 and no deeper than 1.2m in the 1%AEP
- 4. Culverting shall be avoided where possible
- 5. De-culverting is encouraged.
- 6. Examples of Suds systems throughout Fingal available at <u>https://pin.it/yvwrkb3hrekcdu</u>

Flood risk to be assessed

Flood risk	Applicable to subject site	Measures to reduce risk	Residual risk
Fluvial		Refer to Stage 2 Flood Risk Assessment	
Pluvial		Refer to Stage 2 Flood Risk Assessment	
Coastal		Refer to Stage 2 Flood Risk Assessment	
Groundwater		Refer to Stage 2 Flood Risk Assessment	
Dam/Embankment/Canal bank breach		Refer to Stage 2 Flood Risk Assessment	
Network drainage		Refer to Stage 2 Flood Risk Assessment	
Snow melt		Refer to Stage 2 Flood Risk Assessment	
Watermain burst		Refer to Stage 2 Flood Risk Assessment	

Note:

Models should consider the risk when outlets are surcharged

Appendix G



Uisce Éireann Bosca OP 6000 Baile Átha Cliath 1 Éire

Irish Water PO Box 6000 Dublin 1 Ireland

T: +353 1 89 25000 F: +353 1 89 25001 www.water.ie

Jacob Granados Castro The Glass House 11 Coke Lane Smithfield Dublin 7, Dublin D07WNP2

18 February 2019

Dear Jacob Granados Castro,

Re: Connection Reference No CDS19000036 pre-connection enquiry - Subject to contract | Contract denied

Connection for Housing Development of 10 unit(s) at Stokhole Lane, Dublin, Dublin.

Irish Water has reviewed your pre-connection enquiry in relation to a water connection at Stokhole Lane, Dublin.

Based upon the details that you have provided with your pre-connection enquiry and on the capacity currently available in the network(s), as assessed by Irish Water, we wish to advise you that, subject to a valid connection agreement being put in place, your proposed connection to the Irish Water network(s) can be facilitated.

Please be advised that at connection application stage you have to demonstrate that wastewater infrastructure within the Estate is in adequate condition and in compliance with requirements of Irish Water Code of Practice and Standard Details.

You are advised that this correspondence does not constitute an offer in whole or in part to provide a connection to any Irish Water infrastructure and is provided subject to a connection agreement being signed at a later date.

A connection agreement can be applied for by completing the connection application form available at **www.water.ie/connections**. Irish Water's current charges for water and wastewater connections are set out in the Water Charges Plan as approved by the Commission for Regulation of Utilities.

If you have any further questions, please contact Marina Zivanovic Byrne from the design team on 01 89 25991 or email mzbyrne@water.ie. For further information, visit <u>www.water.ie/connections.</u>

Yours sincerely,

M Buyes

Maria O'Dwyer Connections and Developer Services

Stiúrthóirí / Directors: Mike Quinn (Chairman), Eamon Gallen, Cathal Marley, Brendan Murphy, Michael G. O'Sullivan

Oifig Chláraithe / Registered Office: Teach Colvill, 24-26 Sráid Thalbóid, Baile Átha Cliath 1, D01 NP86 / Colvill House, 24-26 Talbot Street, Dublin 1, D01 NP86 Is cuideachta ghníomhaíochta ainmnithe atá faoi theorainn scaireanna é Uisce Éireann / Irish Water is a designated activity company, limited by shares. Uimhir Chláraithe in Éirinn / Registered in Ireland No.: 530363



Uisce Éireann Bosca OP 6000 Baile Átha Cliath 1 Éire

Irish Water PO Box 6000 Dublin 1 Ireland

T: +353 1 89 25000 F: +353 1 89 25001 www.water.ie

Jacob Granados Castro The Glass House 11 Coke Lane Smithfield Dublin 7, Dublin D07WNP2

12 February 2019

Dear Jacob Granados Castro,

Re: Connection Reference No CDS19000030 pre-connection enquiry - Subject to contract | Contract denied

Connection for Housing Development of 7 unit(s) at Stokhole Lane, Dublin, Dublin.

Irish Water has reviewed your pre-connection enquiry in relation to a water connection at Stokhole Lane, Dublin, Dublin.

Based upon the details that you have provided with your pre-connection enquiry and on the capacity currently available in the network(s), as assessed by Irish Water, we wish to advise you that, subject to a valid connection agreement being put in place, your proposed connection to the Irish Water network(s) can be facilitated.

Proposed water connection is via Baskin Estate of 10 no. houses which hasn't been taken in charge. The Estate has water connection from 24' trunk main in Stochole Lane and waste water discharges into a private WWTP which is situated within the proposed site boundaries.

At connection application stage and prior to commencement of any Self-Lay Works:

- The Baskin Estate has to be connected into the gravity sewer in Stochole Lane and existing WWTP with associated pump station and rising main have to be decommissioned and the land decontaminated.
- you should identify and procure transfer to Irish Water of the arterial water Infrastructure within any Third Party Infrastructure
- you should demonstrate that the arterial infrastructure are in compliance with requirements of Irish Water Code of Practice and Standard Details and in adequate condition and capacity to cater for additional load from the Development.

All infrastructure should be designed and installed in accordance with the Irish Water Codes of Practice and Standard Details. A design proposal for the water and/or wastewater infrastructure should be submitted to Irish Water for assessment. Prior to submitting your planning application, you are required to submit these detailed design proposals to Irish Water for review.

You are advised that this correspondence does not constitute an offer in whole or in part to provide a connection to any Irish Water infrastructure and is provided subject to a connection agreement being signed at a later date.

Stiúrthóirí / Directors: Mike Quinn (Chairman), Eamon Gallen, Cathal Marley, Brendan Murphy, Michael G. O'Sullivan

Oifig Chláraithe / Registered Office: Teach Colvill, 24-26 Sráid Thalbóid, Baile Átha Cliath 1, D01 NP86 / Colvill House, 24-26 Talbot Street, Dublin 1, D01 NP86 Is cuideachta ghníomhaíochta ainmnithe atá faoi theorainn scaireanna é Uisce Éireann / Irish Water is a designated activity company, limited by shares. Uimhir Chláraithe in Éirinn / Registered in Ireland No.: 530363 A connection agreement can be applied for by completing the connection application form available at **www.water.ie/connections**. Irish Water's current charges for water and wastewater connections are set out in the Water Charges Plan as approved by the Commission for Regulation of Utilities.

If you have any further questions, please contact Marina Zivanovic Byrne from the design team on 01 89 25991 or email mzbyrne@water.ie. For further information, visit <u>www.water.ie/connections.</u>

Yours sincerely,

M Buye

Maria O'Dwyer Connections and Developer Services

Stiúrthóirí / Directors: Mike Quinn (Chairman), Eamon Gallen, Cathal Marley, Brendan Murphy, Michael G. O'Sullivan Oifig Chláraithe / Registered Office: Teach Colvill, 24-26 Sráid Thalbóid, Baile Átha Cliath 1, D01 NP86 / Colvill House, 24-26 Talbot Street, Dublin 1, D01 NP86 Is cuideachta ghníomhaíochta ainmnithe atá faoi theorainn scaireanna é Uisce Éireann / Irish Water is a designated activity company, limited by shares.

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